

## FORMULATION OF EXPLOITATION CURVES FOR THE TURBINE WITH A HORIZONTAL AXIS

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### **Abstract**

*Formulation of exploitation curves with the turbine with horizontal axis requires employment of an original method to maximize the energy obtained starting from experimental data. Considering the constant values of revolution and the values of wind speed as reference point, the following values have been calculated:  $\lambda$ ,  $C_p$ ,  $P_{arb}$ . Following calculation, certain numerical values have resulted, which have been determined in order to generate a reference point in the subsequent calculations regarding the assessment of energy production for the horizontal turbine which analyzed*

**Key words:** horizontal turbine, exploitation curves, wind speed, the power value, revolution

### **INTRODUCTION**

The exploitation curves for the turbine with a horizontal axis are formulated in relation to the wind speed  $v=3\ldots19\text{m/s}$ , the peripheral speed  $u$ , the air density  $\rho$ , and the exposed area  $S$ , materialized in the formula of unitary power at axis of the turbine::

$$P_{arb} = C_p \cdot \rho \cdot \frac{v^3}{2} \cdot S$$

### **MATERIAL AND METHODS**

The calculation algorithm for the tables below is:

1. speed  $v$  - within the interval  $v=3\ldots19\text{m/s}$  (all the value in the interval)
2. revolution  $n$  – for each table the revolution has been made constant ( $n=50, 100, 150, 200, 250$ )
3. the characteristic number  $\lambda$ :

$$\lambda = \frac{u}{v} = \frac{R \cdot \omega}{v}; \quad \omega = \frac{\pi \cdot n}{30}; \quad \lambda = \frac{R \cdot \pi \cdot n}{30 \cdot v}$$

4. the power value  $C_p$  is calculated using the relation:

$$C_{p_{arb}} = a \cdot \lambda^\alpha - b \cdot \lambda^\beta$$

For the horizontal turbine we use the following values:

$$\alpha=2; \quad a=0,2255$$

$$\beta=3,5; \quad b=0,024805$$

5. power at the axis of the turbine  $P_{arb}$  is calculated using the relation:

$$P_{arb} = C_p \cdot \rho \cdot \frac{v^3}{2} \cdot S$$

For the horizontal turbine we calculate the area exposed to the air using the relation  $S = \frac{\pi \cdot D^2}{4}$ , where  $D = 3,1\text{m}$

Obs.1: We have taken in to consideration the limitation of the power at the axis as  $P_{arb}=3500\text{ W}$ . As a result the figures have been recalculated in the following sequence:

$P_{arb} = 3500 \rightarrow C_p \rightarrow \lambda \rightarrow n$ , using the following formula of calculation:

For the power value we have:

$$C_p = \frac{P_{arb}}{\rho \cdot \frac{v^3}{2} \cdot S}$$

The characteristic number  $\lambda$  has been determined from the graph  $C_{Parb}=f(\lambda)$  using a graphical method (for each calculated  $C_p$ , the correspondence of the characteristic number  $\lambda$  has been determined, by reading the graph).

6. revolution  $n$  – for the power values at the axis  $P_{arb}>3500$  we have calculated the revolution in relation to  $\lambda$  determined from the graph, using the relation  $n = \frac{30 \cdot \lambda \cdot v}{\pi \cdot R}$ .

The results of the calculation  $P_{arb}$  under constant  $n=50\dots250$  rpm. The horizontal turbine:  $\lambda=3$ ,  $C_{Pmax}=0,87$

## RESULTS AND DISCUSSION

### The horizontal turbine

Table 1

The results of the calculation  $P_{arb}$  under constant rotations  $n = 50$

v	n = 50		$P_{arb}$
	$\lambda$	$C_p$	
3	2,71	0,84	110,75
4	2,03	0,63	197,28
5	1,62	0,46	279,29
6	1,35	0,34	358,77
7	1,16	0,26	436,64
8	1,01	0,21	513,44
9	0,90	0,17	589,46
10	0,81	0,14	664,92
11	0,74	0,11	739,93
12	0,68	0,10	814,60
13	0,62	0,08	888,99
14	0,58	0,07	963,15
15	0,54	0,06	1037,12
16	0,51	0,06	1110,94
17	0,48	0,05	1184,62
18	0,45	0,04	1258,18
19	0,43	0,04	1331,64

Table 2

The results of the calculation  $P_{\text{arb}}$  under constant rotations  $n = 100$ 

v	n = 100		$P_{\text{arb}}$
	$\lambda$	$C_P$	
3	5,41	-2,54	-333,51
4	4,06	0,37	116,65
5	3,25	0,85	515,70
6	2,71	0,84	886,00
7	2,32	0,74	1238,23
8	2,03	0,63	1578,25
9	1,80	0,54	1909,54
10	1,62	0,46	2234,36
11	1,48	0,39	2554,20
12	1,35	0,34	2870,14
13	1,25	0,30	3182,93
14	1,16	0,26	3493,15
15	1,08	0,23	3801,23
16	1,01	0,21	4107,51
17	0,95	0,18	4412,27
18	0,90	0,17	4715,72
19	0,85	0,15	5018,02

Table 3

The results of the calculation  $P_{\text{arb}}$  under constant rotations  $n = 150$ 

v	n = 150		$P_{\text{arb}}$
	$\lambda$	$C_P$	
3	8,12	-22,92	-3012,86
4	6,09	-5,45	-1696,89
5	4,87	-0,97	-592,17
6	4,06	0,37	393,69
7	3,48	0,78	1304,89
8	3,04	0,87	2165,58
9	2,71	0,84	2990,24
10	2,43	0,78	3788,10
11	2,21	0,70	4565,43
12	2,03	0,63	5326,58
13	1,87	0,57	6074,74
14	1,74	0,51	6812,26
15	1,62	0,46	7540,96
16	1,52	0,41	8262,23
17	1,43	0,38	8977,19
18	1,35	0,34	9686,72
19	1,28	0,31	10391,54

Table 4

The results of the calculation  $P_{\text{arb}}$  under constant rotations  $n = 200$ 

v	n = 200		$P_{\text{arb}}$
	$\lambda$	$C_P$	
3	10,82	-76,99	-10119,21
4	8,12	-22,92	-7141,59
5	6,49	-7,79	-4742,17
6	5,41	-2,54	-2668,07
7	4,64	-0,48	-798,33
8	4,06	0,37	933,18
9	3,61	0,72	2566,05
10	3,25	0,85	4125,60
11	2,95	0,87	5628,91
12	2,71	0,84	7087,97
13	2,50	0,80	8511,45
14	2,32	0,74	9905,84
15	2,16	0,69	11276,07
16	2,03	0,63	12625,97
17	1,91	0,58	13958,58
18	1,80	0,54	15276,34
19	1,71	0,50	16581,22

Table 5

The results of the calculation  $P_{\text{arb}}$  under constant rotations  $n=250$ 

v	n = 250		$P_{\text{arb}}$
	$\lambda$	$C_P$	
3	13,53	-184,51	-24252,80
4	10,14	-59,28	-18469,32
5	8,12	-22,92	-13948,42
6	6,76	-9,64	-10137,93
7	5,80	-4,06	-6773,66
8	5,07	-1,49	-3711,26
9	4,51	-0,24	-864,27
10	4,06	0,37	1822,63
11	3,69	0,68	4386,73
12	3,38	0,81	6854,18
13	3,12	0,86	9243,96
14	2,90	0,87	11570,20
15	2,71	0,84	13843,68
16	2,54	0,81	16072,78
17	2,39	0,76	18264,12
18	2,25	0,72	20423,03
19	2,14	0,68	22553,84

The graph below displays the correspondence between speed and power at the axis for the rotations presented with colored symbols in the corresponding legend.

These curves are formulated in relation to wind speed  $v$ , peripheral speed  $u$ , air density  $\rho$  and the exposed area ( $S = \pi \cdot D^2 / 4$ ). The following strategy has been used: at the level of installed power by setting a constant rotation, the power at the axis of the turbine has been limited to the value  $P_{arb}=3500$  W.

We have defined the correspondences  $P_{arb}=f(v)$  for the rotations analyzed ( $n = 50 \dots 250$ ), These rotations are set in the mode of operation of the horizontal assembly.

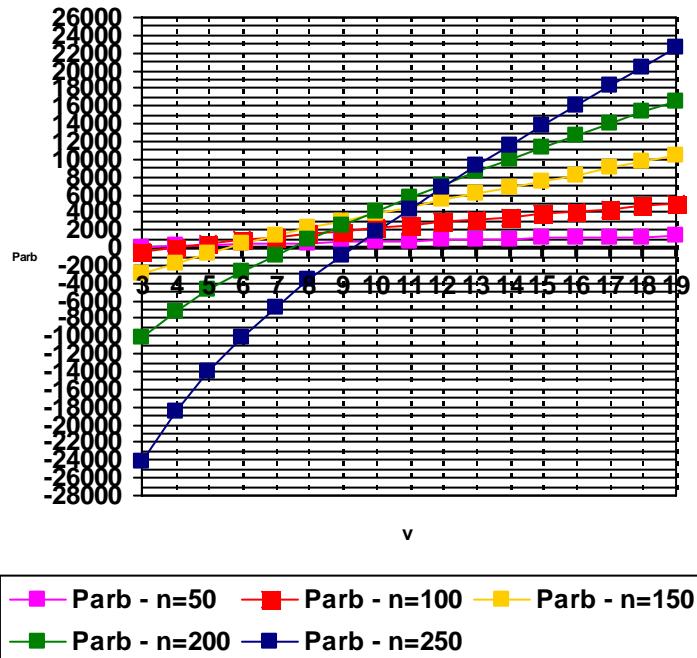


Fig. 1. The correspondence between speed and power at the axis for the rotations presented with colored symbols in the legend above

## CONCLUSIONS

It can be noticed that according to the constant revolution which has been analyzed, at a certain value of wind speed it is essential to limit the power at the axis of the turbine mentioned before. For revolutions  $n = 50, 100$ , the limitation of power was not necessary, while for the other revolutions which were analyzed,  $n = 150, 200, 250$  it was necessary to limit the power at the respective values of wind speed.

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